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[^0]practice section 816177
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# 6177 4Wire-to-2Wire SF-to-FXS Intermediate Repeater 

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## 1. general description

1.01 The 6177 4Wire-to-2Wire SF-to-FXS Intermediate Repeater module (figure 1) provides both active transmission interface and bidirectional signaling conversion between a 4wire facility that uses 2600 Hz single-frequency (SF) signaling and a 2 wire metallic link (station loop or PBX trunk) that uses foreign-exchange station-end (FXS) loop signaling. This type of loop signaling is normally associated with the station end of both foreignexchange (FX) and off-premises-station (OPS) circuits. The 6177 is designed in accordance with the specifications given in AT\&T Technical Reference Pub 43001: Functional Criteria for Voice-Frequency Terminating Equipment/Metallic Facilities/Central Office.
1.02 In the event that this practice section is revised or reissued, the reason for revision or reissue will be stated in this paragraph.
1.03 The 6177 module offers the following features and options:

- 4wire-to-2wire conversion via an integral magnetic hybrid.
- From 0 to 24 dB of prescription-set gain or loss, in switch-selectable 0.1 dB increments, in both the transmit and receive channels at the facility-side 4 wire ports.
- From 0 to 24 dB of prescription-set loss, in switch-selectable 0.1 dB increments, in both the transmit and receive channels on the module's terminal (2wire) side. This loss is actually introduced on the 4wire side of the hybrid.
- Active prescription slope-type or bump-type amplitude equalization, equivalent to that provided by the Western Electric (WECo) 309B Prescription Equalizer, in the receive channel.
- Isolation transformers that are center-tapped to derive balanced simplex (SX) leads at both facility-side 4wire ports.
- Independently switch-selectable 1200, 600, or 150 -ohm terminating impedance at each facilityside 4wire port.
- Switch-selectable 900 or 600 -ohm terminating impedance in series with $2.15 \mu \mathrm{~F}$ at the terminalside 2 wire port.
- Integral 2600 Hz SF tone oscillator.

figure 1. 61774 Wire-to-2Wire SF-to-FXS Intermediate Repeater module
- Switch-selectable loop-start or ground-start operation.
- Switch-selectable automatic ringdown operation as an alternative to FXS operation.
- Integral compromise balance network (CBN) with switch-selectable 900 or 600-ohm impedance in series with $2.15 \mu \mathrm{~F}$ of capacitance.
- Integral precision balance network (PBN) functionally equivalent to either the WECo 4240B PBN (for nonloaded cable) or the WECo 4240C PBN (for loaded cable), as selected via switch option.
- From 0 to $0.126 \mu \mathrm{~F}$ of line build-out capacitance (LBOC) in switch-selectable $0.002 \mu \mathrm{~F}$ increments.
- Minimum-break transmit pulse correction.
- Traffic-monitoring (sleeve) lead.
- Loop-current limiting.
- Front-panel LED that lights to indicate busy.
- Lightning surge protection at all transmission ports.
- Reverse-battery protection, transient-limiting circuitry, and RC (resistance-capacitance) filtering and decoupling networks to minimize crosstalk coupling and the effects of noise on the input power leads.
- Operation on filtered, ground-referenced -42 to -54 Vdc input power with current requirements of 75 mA typical at idle (at -48 Vdc ) and 126 mA maximum (at -54 Vdc ), not including loop current and with one channel at maximum output.
- Type 10 module for mounting in a variety of Tellabs Type 10 Mounting Shelves, which are available in versions for relay-rack (occupying 6 inches of vertical rack space) and apparatuscase installation.


## 2. application

2.01 The 6177 4Wire-to-2Wire SF-to-FXS Intermediate Repeater module is designed primarily to interface a 4wire transmission facility that uses SF signaling with a 2 wire metallic link that uses FXS signaling. This link can be either a station loop or a PBX trunk (loop-start or ground-start) that terminates at the station end of an FX or OPS circuit. The 6177 module combines the functions of a 4wire line amplifier, an SF transceiver, an SF-to-FXS signaling converter, and a 4wire-to-2wire hybrid terminating set. No external interface circuitry is required because the 6177 is a complete SF signaling and terminating circuit, less power and ringing, on a single Type 10 card. Thus, the module provides not only bidirectional signaling conversion but also active transmission interface (impedance matching, level control, amplitude equalization, and 4wire-to2 wire conversion) between the SF facility and the FXS link. Figures 2 and 3 show typical applications.
terminal (2wire) interface, balance network, and line build-out capacitance (LBOC)
2.02 The 6177 interfaces the 2 wire station loop or PBX trunk via prescription attenuators in the transmit and receive paths on the 4wire side of the integral magnetic hybrid (see paragraph 2.07) and via the hybrid itself. This hybrid provides switchselectable 900 or 600 -ohm terminating impedance (in series with $2.15 \mu \mathrm{~F}$ ) at the 2 wire port. The $900-$ ohm option is selected for interface with loaded cable (or with a switched network involving both loaded and nonloaded cable). The 600-ohm option
is selected for interface with nonloaded cable or station equipment. To ensure that adequate hybrid balance (i.e., enough transhybrid loss) is provided, the module's internal compromise balance network (CBN) or internal precision balance network (PBN) can be switched-optioned to function with the hybrid.
2.03 Compromise Balance Network (CBN). With the internal CBN selected, the 2wire-port impedance switch automatically selects the same impedance for the CBN as is selected for the 2wire port: 600 or 900 ohms in series with $2.15 \mu \mathrm{~F}$. If the CBN does not provide adequate hybrid balance (i.e., sufficient transhybrid loss), use of the PBN is required.
2.04 Precision Balance Network (PBN). When the internal CBN does not provide adequate transhybrid balance, the internal PBN can be selected instead. This internal PBN can be switchoptioned for use with loaded cable, in which case it is functionally equivalent to the Western Electric (WECo) 4240C PBN, or for use with nonloaded cable, in which case it is functionally equivalent to the WECo 4240B PBN. When optioned to balance nonloaded cable, the PBN operates as follows:

- The $Z$ switches affect impedance equally at all frequencies.
- The $R / R 1$ switches affect impedance at low frequencies.
- The R2 switches affect impedance at midband frequencies.

figure 2. Typical foreign-exchange (FX) application of 6177 module

figure 3. Typical off-premises-station (OPS) application of 6177 module

When optioned to balance loaded cable, the PBN operates as follows:

- The Z switches affect impedance at all frequencies.
- The R/R1 switches affect impedance at low frequencies.
- The R2 switches are nonfunctional.
2.05 Line Build-Out Capacitance (LBOC). To further improve hybrid balance, especially in applications where the PBN is optioned for loaded cable, from 0 to $0.126 \mu \mathrm{~F}$ of line build-out capacitance (LBOC) can be introduced across the hybrid's 2wire port. Generally, LBOC is not used when the PBN is optioned for nonloaded cable.


## facility (4wire) interface

2.06 The 6177 interfaces the facility-side 4wire SF signaling facility via prescription amplifiers in the transmit and receive paths (see paragraph 2.07) and via transformers at the transmit output and receive input ports. Each facility-side transformer provides balanced, switch-selectable 1200, 600, or 150 -ohm terminating impedance. The 1200 -ohm option is used for interface with loaded cable; the 600 -ohm option, for interface with nonloaded cable or carrier; and the 150 -ohm option, to provide a small amount of slope-type amplitude equalization for nonloaded cable through the deliberate impedance mismatch. Both facility-side transformers are center-tapped to derive simplex (SX) leads, which can be used to provide sealing current to a metallic facility from a local source external to the module, or which can be strapped together to establish a return path for sealing current applied at the distant end of the facility.

## level control

2.07 Prescription-set transmit and receive amplifiers on the facility side of the 6177 allow the module to interface the 4wire SF signaling facility directly, i.e., without a separate facility-side line amplifier. These amplifiers, in conjunction with the prescription-set transmit and receive attenuators on the module's terminal side, provide for full coordination between facility-side ( 4 wire) and terminal-side ( 2 wire) levels (see figure 4). In the receive channel, the facility-side amplifier is set to provide the gain or loss necessary to derive a +7 transmission level point (TLP) within the module. This internal TLP is then used as a reference as the module's terminalside receive attenuator is set to provide the loss necessary to derive the required terminal-side 2 wire output level. In the transmit channel, the terminal-side attenuator is set to provide the loss necessary to derive a -16TLP within the module. This internal TLP is then used as a reference as the module's facility-side transmit amplifier is set to provide the gain or loss necessary to derive the required facility-side 4 wire transmit output level. Both facility-side amplifiers in the 6177 provide from 0 to 24 dB of gain or 0 to 24 dB of loss in switchselectable 0.1 dB increments. Both terminal-side attenuators provide from 0 to 24 dB of loss in switch-selectable 0.1 dB increments. Thus, 4wire receive TLP's from -17 to +7 can be accommodated and 2 wire output TLP's from +7 to -17 can be derived. In a similar manner, 2 wire input TLP's from -16 to +8 can be accommodated and 4 wire transmit TLP's from +8 to -16 can be derived. Total facility-side gain or loss and total terminal-side loss introduced into a channel are the

figure 4. Level coordination in 6177 module
respective sums of that channel's front-panel fac level and term loss switches set to $I N$. The overload point for the 4 wire receive port and the 2 wire port output is OdBmO. The overload point for the 2 wire port input and the 4 wire transmit port is +3 dBmo .

## receive-channel amplitude equalization

2.08 Active prescription amplitude equalization functionally equivalent to that provided by the Western Electric 309B Prescription Equalizer is available in the receive channel of the 6177 for postequalization of the 4 wire receive pair. This equalizer provides low-end slope equalization down to 404 Hz and high-end bump equalization centered at 3250 Hz for loaded or nonloaded cable, as selected via switch option. Degree of slope, height of bump, and affected bandwidth are also controlled by option switches on the module. If no equalization is required, the equalizer can be electrically bypassed by means of another switch option.
2.09 Figures 5 and 6 show typical response curves for the 309B-equivalent equalizer in the slope mode. Figure 5 shows the curves for nonloaded cable, while figure 6 shows the curves for loaded cable. For comparison purposes, all fre-quency-response curves in both figures are drawn with the same 0 dB -gain reference point $(1004 \mathrm{~Hz})$.

figure 5. Typical response curves for receive equalizer in slope mode, nonloaded cable

figure 6. Typical response curves for receive equalizer in slope mode, loaded cable

Actually, all of these curves except those for a SLOPE switch setting of 0 are raised above the OdB level at 1004 Hz by as much as 11.4 dB . The exact amount by which a particular curve is raised depends upon the SLOPE and NL (nonloaded/ loaded) switch settings selected. These amounts are listed in table 1.

| SLOPE switch setting | L/NL (loaded/nonloaded) switch setting |  |
| :---: | :---: | :---: |
|  | L | NL |
| 0 (slope disabled) | 0.0 dB | 0.0 dB |
| 1 | 1.4 | 0.4 |
| 2 | 2.6 | 0.9 |
| 3 | 3.7 | 1.4 |
| 4 | 4.7 | 1.8 |
| 5 | 5.5 | 2.3 |
| 6 | 6.3 | 2.8 |
| 7 | 7.2 | 3.4 |
| 8 | 7.8 | 3.7 |
| 9 | 8.4 | 4.2 |
| 10 | 9.0 | 4.6 |
| 11 | 9.5 | 5.0 |
| 12 | 10.0 | 5.4 |
| 13 | 10.5 | 5.8 |
| 14 | 11.0 | 6.2 |
| 15 | 11.4 | 6.6 |

table 1. Equalized gain (in dB) at 1004 Hz in slope mode
2.10 Figures 7 and 8 show typical response curves for the 309B-equivalent equalizer in the bump mode. Figure 7 shows the curves representing various height settings versus a wide bandwidth setting, while figure 8 shows the curves representing various height settings versus a narrow bandwidth setting. For comparison purposes, all fre-quency-response curves in both figures are drawn with the same OdB-gain reference point $(1004 \mathrm{~Hz}$ ). Actually, all of these curves except those for a height (HT) switch setting of 1 or 0 and/or for a bandwidth ( $B W$ ) switch setting of 5 or less are raised above the OdB level by as much as 3.9 dB . The exact amount by which a particular curve is raised depends upon the $H T$ and $B W$ switch settings selected. These amounts are listed in table 2.

figure 7. Typical response curves for receive equalizer in bump mode, BW switch $=14$

| HT switch setting* | BW switch setting** |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| 2 | 0.0 dB | 0.0 dB | 0.0 dB | 0.0 dB | 0.0 dB | 0.0 dB | 0.0 dB | 0.1 dB | 0.1 dB | 0.2 dB |
| 3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 01 | 03 |
| 4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 | 0.2 | 0.4 |
| 5 | 00 | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 | 0.1 | 02 | 03 | 0.5 |
| 6 | 0.0 | 0.0 | 0.1 | 0.1 | 0.1 | 0.1 | 0.2 | 0.2 | 0.4 | 07 |
| 7 | 00 | 0.1 | 0.1 | 0.1 | 0.1 | 0.2 | 0.2 | 0.3 | 0.5 | 0.9 |
| 8 | 0.0 | 0.1 | 0.1 | 01 | 0.2 | 0.2 | 03 | 0.4 | 0.7 | 12 |
| 9 | 0.0 | 0.1 | 0.1 | 0.2 | 0.2 | 0.3 | 04 | 0.5 | 0.8 | 1.5 |
| 10 | 0.1 | 0.1 | 02 | 0.2 | 0.2 | 03 | 0.4 | 0.6 | 1.0 | 17 |
| 11 | 0.1 | 0.1 | 0.2 | 0.2 | 0.3 | 0.4 | 0.5 | 0.7 | 12 | 2.0 |
| 12 | 01 | 01 | 0.2 | 03 | 0.3 | 0.4 | 0.6 | 0.9 | 14 | 2.4 |
| 13 | 0.1 | 0.2 | 0.3 | 0.3 | 0.4 | 0.6 | 0.8 | 1.1 | 17 | 2.8 |
| 14 | 0.1 | 02 | 0.3 | 0.4 | 0.5 | 0.7 | 0.9 | 1.3 | 2.0 | 3.3 |
| 15 | 0.2 | 0.3 | 0.4 | 0.5 | 0.7 | 0.9 | 1.2 | 1.7 | 2.5 | 39 |

* An HT switch setting of 0 disables the bump function. An HT switch setting of 1 introduces 0.1 dB of gain or less at 1004 Hz * A $B W$ switch setting of 0 through 5 introduces $O .1 d B$ of gain or less for all $H T$ switch settings.
table 2. Equalized gain (in $d B$ ) at 1004 Hz in bump mode

figure 8. Typical response curves for receive equalizer in bump mode, BW switch $=3$


## supervisory states, loop start

2.11 The 6177 module accommodates a conventional loop-start supervisory format. In loop-start operation, detection of incoming SF tone activates ringing toward the station or PBX trunk circuit. Loop current is supplied to the station-side loop or trunk through matched resistances in the module's A\&B leads.

## supervisory states, ground start

2.12 In ground-start operation, just as in loopstart, the 6177 module accommodates a conventional supervisory format. Whenever incoming SF tone is detected, the 2 wire tip-lead path is opened to ground, except during ringing. Presence of SF tone at the 4 wire receive port indicates that the associated office-end circuit is idle (2wire tip lead open), and local ringing is initiated by receipt of SF tone amplitude-modulated by a ringing frequency of 18 to 33 Hz . Outgoing seizure is initiated in groundstart operation by application of ground to the 2 wire ring lead, which causes transmission of SF tone to cease.

## loop-current limiting and supervisory limits

2.13 An internal loop-current limiter on the 6177 limits current to less than approximately 35 mA on short loops. With long loops, at least 16 mA of current must be drawn from the battery feed to guarantee proper operation. In ground-start operation, the module senses application of ground to the 2wire ring lead to initiate seizure toward the distant end. The ring-ground sensor in the 6177 can sense application of this ground through external resistance of up to 3000 ohms on the 2 wire ring lead.

## ring trip and ring-trip range

2.14 The 6177 provides for removal of local ringing when the station or PBX trunk responds to incoming seizure. For proper operation of the ringtrip circuit, the external ringing source must be referenced to a potential of -42 to -54 Vdc . The 6177 can reliably detect ring trip at up to 2000 ohms of external loop resistance with -48 Vdc biased ringing.

## signaling-tone states

2.15 Signaling-tone states for the 6177 are consistent with the conventional F-signaling formats of FXS and station-end OPS service. These states are listed in tables 3 and 4 for loop-start and groundstart operation, respectively.

## incoming SF tone detection

2.16 The 6177 is designed to interface the receive path on the facility (4wire) side at any TLP from -17 to +7 . Idle-state SF tone is received at a level of -20 dBmo . A higher level of -8 dBmO is received during break portions of dial pulses and for about 400 ms at the beginning of each tone interval. The 6177's SF tone detector reliably detects tone levels as low as -27 dBmO , provided that the SF tone energy is approximately 12 dB above the level of all other signals simultaneously present at the 4 wire receive port. The SF tone detector is actually a signal-to-guard ratio comparator that compares energy in a narrow band of frequencies centered at the SF tone frequency with energy in the entire voice band. This detection
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| local loop <br> condition | SF tone |  |
| :--- | :---: | :---: |
|  | receive | transmit |
| idle | off | on |
| ringing | on | on |
| off-hook | off | off |
| dialing | off | off-on-off |

table 3. Loop-start signaling-tone states

| local loop <br> condition | SF tone |  |
| :--- | :---: | :---: |
|  | receive | transmit |
| seizure from CO | on | on |
| ringing | off | on |
| busy | off-on-off | on |
| CO release | off | off |
| idle | off until detection <br> of incoming SF <br> tone, then on |  |
| local seizure | on | on |
| CO seizure <br> acknowledgement | on | off |
| dialing | off | off |
| busy | off | off-on-off |
| local station <br> disconnect first | off | off |
| CO release | on | on |
| idle | on | on |

table 4. Ground-start signaling-tone states
arrangement aids significantly in prevention of talkoff, but it places an upper bound on allowable circuit noise. In general, received noise in excess of 51dBrnC0 may interfere with detection of low-level signaling tones.
2.17 The 6177's SF tone detector is designed to ignore momentary losses of SF tone during periods of otherwise continuous receipt of tone and to ignore momentary tone bursts to prevent false signaling. Within approximately 13 ms of detection of incoming SF tone, a band-elimination filter (BEF) is inserted into the receive transmission path to prevent propagation of SF tone beyond the module. An internal timing circuit ensures that the filter remains inserted during dial pulsing and during momentary losses of tone continuity.

## outgoing SF tone transmission

2.18 The 6177 is designed to interface the transmit path on the facility (4wire) side at any TLP from +8 to -16 . During the idle state, the module transmits SF tone at -20 dBm . During dial pulsing and also for the first 400 ms each time it applies tone to the facility, the module transmits SF tone at a higher level of -8 dBm . This momentarily increased tone level aids in office-end detection of supervisory-state changes and incoming dial pulsing.

## delay circuit and transmit pulse correction

2.19 The 6177 contains a delay circuit in the loop-current sensor that delays detection of on-hook-to-off-hook and off-hook-to-on-hook transitions by about 18 ms to prevent false detection of
short transients typically associated with station loops. A minimum-break pulse corrector in the transmit path ensures a 50 ms minimum break duration and a 25 ms minimum make duration during dialing, regardless of input break or pulsing rate. The minimum-break pulse corrector has no effect upon pulsing breaks longer than 50 ms .

## transmit path cut

2.20 To prevent speech and transient energy from interfering with detection of SF signaling tone at the distant end of the circuit, the voice path through the transmit portion of the 6177 is cut (opened) during dialing and whenever SF tone is transmitted or received.

## automatic ringdown operation

2.21 As an alternative to FXS operation, the 6177 can be switch-optioned to operate in a loop-start or ground-start automatic-ringdown circuit. In such applications, two 6177's connected to telephone sets are used at each end of a circuit. In the idle (on-hook) condition, SF tone is sent, while off-hook conditions are indicated by no tone. If either telephone goes off-hook, the distant-end telephone rings, and ringback tone is sent to the calling 6177 until the station is answered. The ringing rate in the auto-ringdown mode is fixed at 2 seconds on and 4 seconds off. The 6177 can also be used in the autoringdown mode to interface a conventional E\&M SF facility, i.e., one with tone on in both directions during idle.

## SF tone source

2.22 The module is equipped with an integral 2600 Hz SF tone oscillator and therefore does not require an associated master SF tone supply.

## power

2.23 The 6177 is designed to operate on filtered, ground-referenced input potentials between -42 and -54 Vdc . The positive side of the dc power supply must be connected to earth ground. Groundstart operation of the station-end equipment (e.g., PBX or telephone set) requires a low-resistance ground that is common with the ground of the module. Maximum current required at -54 Vdc is 126 mA , not including loop current and with one channel at maximum output.

## ringing

2.24 The ringing circuits in the 6177 operate with any ringing frequency between 16 and 67 Hz , but the ringing generator must be referenced to (or superimposed upon) a potential of -42 to -54 Vdc for reliable operation of the ring-trip detector. In the ground-start mode, the module responds to any ringing frequency (modulated SF tone) between 18 and 33 Hz .

## traffic monitoring

2.25 The 6177 permits traffic monitoring of circuit seizures via a traffic-monitoring output lead (pin 1) that functions much like a local sleeve lead. This lead provides a ground output when the local station is off-hook and also during the break portion of dial pulses. When the circuit is idle, the lead is open.

## 3. installation <br> inspection

3.01 The 6177 4Wire-to-2Wire SF-to-FXS Intermediate Repeater module should be visually inspected upon arrival to find any damage incurred during shipment. If damage is noted, a claim should immediately be filed with the carrier. If stored, the module should be visually inspected again prior to installation.

## mounting

3.02 The 6177 mounts in one position of a Tellabs Type 10 Mounting Shelf. The module plugs physically and electrically into a 56-pin connector at the rear of its shelf position.

## installer connections

3.03 When a 6177 module is to be installed in a non-prewired Type 10 Shelf, external connections to the module must be made. Before making any connections to the shelf, ensure that power is off and modules are removed. Modules should be put into place only after they are properly optioned and after wiring is completed.
3.04 Table 5 lists external connections to the 6177. All connections to non-prewired mountings are made via wire-wrapping to the 56-pin connector at the rear of the module's shelf position. Pin numbers are found on the body of the connector.

| connect: | to pin: |
| :---: | :---: |
| 4WIRE RCV TIP | 7 |
| 4WIRE RCV RING | 13 |
| 4WIRE XMT TIP | 41 |
| 4WIRE XMT RING | 47 |
| 2WIRE TIP | 55 |
| 2WIRE RING | 49 |
| 4WIRE RCV SX (simplex, facility side) | 9 |
| 4WIRE XMT SX (simplex, facility side) | 43 |
| A lead | 51 |
| B lead | 3 |
| SLEEVE (traffic-monitoring or sleeve lead) . |  |
| MACHINE START (ringing machine start lead) | 30 |
| RING GEN (ringing generator) | 46 |
| -BATT (-42 to -54Vdc filtered input) | 35 |
| GND (ground) | 17 |

table 5. External connections to 6177

## option selection

3.05 Several option switches must be set before the 6177 is placed into service. Locations of these switches and of certain alignment switches on the module's printed circuit board are shown in figure 9. Table 6 summarizes all switch options and provides a convenient checklist that can be filled out either prior to installation for prescription optioning or during installation to serve as a record for later reference. Refer to figure 9 and table 6, and set each option switch on the 6177 as required.

figure 9. 6177 option switch locations

## alignment overview

3.06 Alignment of the 6177 module comprises the following procedures (all option switches should already be properly set as described above):
A. Setting the receive-channel facility-side and terminal-side levels.
B. Introducing receive-channel equalization, if necessary.
C. Setting the transmit-channel terminal-side and facility-side levels.
D. Either inserting and optioning the integral CBN (if not already done), or inserting and aligning the integral PBN, if necessary.
E. Introducing line build-out capacitance (LBOC) on the terminal side, if necessary.

## prescription alignment

3.07 The 6177 module is primarily intended for prescription alignment. This involves setting all level-control, equalization, balance-network, and LBOC switches in accordance with specifications on the circuit layout record (CLR) before plugging the module into its shelf position. Table 7 in this practice summarizes all alignment switches on the 6177 and provides a convenient checklist for prescription alignment. To use this table, simply indicate all required alignment-switch settings in the checklist column. Then, at installation time, align the 6177 by setting each switch as indicated in the table (or on the CLR, if preferred).
Note: Prescription alignment procedures for the precision balance network (PBN) can be found in Bell System Practice (BSP) section 332-912-222. Manual alignment procedures for the $P B N$ can be found in BSP section 332-912-221.
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| option | switch | selection | setting | checklist |
| :---: | :---: | :---: | :---: | :---: |
| terminating impedance, 4wire receive port (facility side) | RCVIN IMPD (S1) switches (lefthand 150 and 600 switches) on main board | 1200 ohms (for loaded cable) | 150 switch toward 1200, 600 switch toward 1200 |  |
|  |  | 600 ohms (for nonloaded cable or carrier) | 150 switch toward 1200, 600 switch toward 600 |  |
|  |  | 150 ohms (extra equalization for nonloaded cable) | 150 switch toward 150. 600 switch toward 1200 |  |
| terminating impedance, 4wire transmit port (facility side) | XMT OUT IMPD (S1) switches (righthand 150 and 600 switches) on main board | 1200 ohms (for loaded cable) | 150 switch toward 1200, 600 switch toward 1200 |  |
|  |  | 600 ohms (for nonloaded cable or carrier) | 150 switch toward 1200, 600 switch toward 600 |  |
|  |  | 150 ohms (extra equalization for nonioaded cable) | 150 switch toward 150, 600 switch toward 1200 |  |
| terminating impedance, 2wire port (terminal side)* | 2W IMPD switch (S3) on main board) ${ }^{\star}$ | 900 ohms plus $2.15 \mu \mathrm{~F}$ | 900 |  |
|  |  | 600 ohms plus $2.15 \mu \mathrm{~F}$ | 600 |  |
| loop-start or ground-start operation | LS/GS switch (S12) on baby board | loop start | LS |  |
|  |  | ground start | GS |  |
| automatic ringdown or FXS application | ARD/FXS switch (S15) on baby board | automatic ringdown | ARD |  |
|  |  | FXS | FXS |  |
| balance network selection | LD/NL/CBN switch (S24) on main board | PBN, loaded cable | LD |  |
|  |  | PBN, nonloaded cable | NL |  |
|  |  | CBN | CBN |  |

* With the module's integral CBN optioned into the circuit via switch S24, switch S3 automatically selects the same impedance for the CBN as is selected for the 2 wire port.
table 6. Summary and checklist of 6177 switch options


## 4. circuit description

4.01 To provide the clearest possible understanding of the operation of the 6177 4Wire-to-2Wire SF-to-FXS Intermediate Repeater module, function sequence flowcharts (figures 10 and 11) that illustrate operation of the module on incoming and outgoing calls are presented in lieu of a more conventional circuit description. Horizontal paths identify events occurring simultaneously, and vertical paths denote sequential events. Dotted lines indicate elapsed time. These flowcharts can be used to determine normal operation by observing the module's response and comparing it to that shown in the flowcharts. Reference to the 6177 block diagram (section 5 of this practice) will aid in understanding the flowcharts.
4.02 The flowcharts are intended to familiarize you with the operation of the 6177 for engineering, application, and troubleshooting purposes only. Attempts to test or troubleshoot this module internally are not recommended and may void its Tellabs warranty. Procedures for recommended testing and troubleshooting in the field should be limited to those prescribed in section 7 of this practice.

## 6. specifications

## transmission

alignment level ranges, facility-side ports
4wire rcv port: -17 to +7TLP
4 wire xmt port: $\mathbf{- 1 6}$ to +8 TLP
alignment level ranges, 2 wire port
2wire-port output: +7 to -17TLP
2wire-port input: +8 to -16 TLP
overload points
4wire rcv port: OdBm0
4wire xmt port: $+3 \mathrm{dBm0}$
2wire-port output: OdBmO
2wire-port input: +3dBm0
facility-side gain or loss (xmt and rcv)
0 to 24 dB of gain or 0 to 24 dB of loss in switch-
selectable 0.1 dB increments, with gain or loss selected via switch option
terminal-side loss (xmt and rcv)
0 to 24 dB of loss in switch-selectable 0.1 dB increments
insertion loss, xmt and rcv channels
(600-ohm termination at all ports)
$0 \pm 0.2 \mathrm{~dB}$ at 1004 Hz with all level-control switches set for no gain or loss

| alignment function | switch | selection | setting | checklist |
| :---: | :---: | :---: | :---: | :---: |
| selection of receive-channel facility-side flat gain or loss | GN and LS positions of front-panel rcv fac level DIP switch | gain | GN to IN LS to OUT |  |
|  |  | loss | GN to OUT LS to IN |  |
| ```amount of receive-channel facility-side gain or loss, as selected above*``` | dB -value positions of front-panel rcv fac level DIP switch* | 0.1 dB | . 1 to IN |  |
|  |  | 0.2 dB | . 2 to IN |  |
|  |  | 0.4 dB | . 4 to IN |  |
|  |  | 0.8 dB | . 8 to IN |  |
|  |  | 1.5 dB | 1.5 to IN |  |
|  |  | 3.0 dB | 3 to IN |  |
|  |  | 6.0 dB | 6 to IN |  |
|  |  | 12.0 dB | 12 to IN |  |
| receive-channel terminal-side flat loss* | front-panel rcv term loss DIP switch* | 0.1 dB | . 1 to IN |  |
|  |  | 0.2 dB | 2 to IN |  |
|  |  | 0.4 dB | 4 to IN |  |
|  |  | 0.8 dB | . 8 to IN |  |
|  |  | 1.5 dB | 1.5 to IN |  |
|  |  | 3.0 dB | 3 to IN |  |
|  |  | 6.0 dB | 6 to IN |  |
|  |  | 12.0 dB | 12 to IN |  |
| inclusion or bypass (exclusion) of receive-channel (post-) equalizer | IN/OUT position of frontpanel rcv equalizer SLOPE DIP switch | equalizer included in circuit | IN |  |
|  |  | equalizer bypassed (excluded) | OUT |  |
| introduction of receivechannel 309B-equivalent equalization | SLOPE NL position of front-panel rcv equalizer SLOPE DIP switch | nonloaded cable | toward NL |  |
|  |  | loaded cable | away from NL |  |
|  | SLOPE 1, 2, 4, 8 positions of front-panel rcv equalizer SLOPE DIP switch ${ }^{\star *}$ | degree of slope | SLOPE 1 to 1 |  |
|  |  |  | SLOPE 2 to 2 |  |
|  |  |  | SLOPE 4 to 4 |  |
|  |  |  | SLOPE 8 to 8 |  |
|  | HT 1, 2, 4, 8 positions of front-panel rcv equalizer HT/BW DIP switch** | height of bump | HT 1 to 1 |  |
|  |  |  | HT 2 to 2 |  |
|  |  |  | HT 4 to 4 |  |
|  |  |  | HT 8 to 8 |  |
|  | BW 1, 2, 4, 8 positions of front-panel rcv equalizer HT/BW DIP switch** | affected bandwidth | BW 1 to 1 |  |
|  |  |  | BW 2 to 2 |  |
|  |  |  | BW 4 to 4 |  |
|  |  |  | BW 8 to 8 |  |
| selection of transmit-channel facility-side flat gain or loss | GN and LS positions of front-panel xmt fac level DIP switch | gain | GN to IN LS to OUT |  |
|  |  | loss | GN to OUT LS to IN |  |
| amount of transmit channel facility-side gain or loss, as selected above* | dB-value positions of front-panel xmt fac level DIP switch* | 0.1 dB | . 1 to IN |  |
|  |  | 0.2 dB | . 2 to IN |  |
|  |  | 0.4 dB | . 4 to IN |  |
|  |  | 0.8 dB | . 8 to IN |  |
|  |  | 1.5 dB | 1.5 to IN |  |
|  |  | 3.0 dB | 3 to IN |  |
|  |  | 6.0 dB | 6 to IN |  |
|  |  | 12.0 dB | 12 to IN |  |
| transmit-channel terminal-side flat loss* | front-panel xut term loss DIP switch* | 0.1 dB | . 1 to IN |  |
|  |  | 0.2 dB | . 2 to IN |  |
|  |  | 0.4 dB | . 4 to IN |  |
|  |  | 0.8 dB | . 8 to IN |  |
|  |  | 1.5 dB | 1.5 to IN |  |
|  |  | 3.0 dB | 3 to IN |  |
|  |  | 6.0 dB | 6 to IN |  |
|  |  | 12.0 dB | 12 to IN |  |

table $\mathbf{7}$ continued on next page

| alignment function | switch | selection | setting | checklist |
| :---: | :---: | :---: | :---: | :---: |
| precision balance network (PBN) alignment, loaded-cable applications (S24 set to $L D$ ) | L position of R/R1 (S26) on main board | MAT cable (low-capacitance loaded cable) | L to IN |  |
|  |  | high-capacitance loaded cable | L to OUT |  |
|  | $Z$ (S25) on main board*** | 1 | 1 to IN |  |
|  |  | 2 | 2 to IN |  |
|  |  | 4 | 4 to IN |  |
|  |  | 8 | 8 to IN |  |
|  |  | 16 | 16 to IN |  |
|  | 1,2, and 4 positions of $R /$ $R 1$ (S26) on main board** | 1 | 1 to IN |  |
|  |  | 2 | 2 to IN |  |
|  |  | 4 | 4 to IN |  |
|  | R2 (S27) on main board | NO SELECTION AVAILABLE: all four positions of $R 2$ are nonfunctional with S24 set to $L D$ | DON'T CARE |  |
| line build-out capacitance (LBOC), terminal side, loaded-cable applications (S24 set to LD) | LBOC (S8) on main board, $\mu \mathrm{F} / 1000^{* * *}$ | $0.002 \mu \mathrm{~F}$ | 2 to IN |  |
|  |  | $0.004 \mu \mathrm{~F}$ | 4 to lN |  |
|  |  | $0.008 \mu \mathrm{~F}$ | 8 to IN |  |
|  |  | $0.016 \mu \mathrm{~F}$ | 16 to IN |  |
|  |  | $0.032 \mu \mathrm{~F}$ | 32 to IN |  |
|  |  | $0.064 \mu \mathrm{~F}$ | 64 to IN |  |
| precision balance network (PBN) alignment, nonloaded-cable applications (S24 set to NL) | L position of R/R1 (S26) on main board | NO SELECTION AVAILABLE: $L$ position of $R / R 1$ is nonfunctional with S24 set to NL | DON'T CARE |  |
|  | $Z$ (S25) on main board*** | 1 | 1 to IN |  |
|  |  | 2 | 2 to N |  |
|  |  | 4 | 4 to IN |  |
|  |  | 8 | 8 to IN |  |
|  |  | 16 | 16 to IN |  |
|  | 1, 2, and 4 positions of $R / R 1$ (S26) on main board*** | 1 | 1 to IN |  |
|  |  | 2 | 2 to IN |  |
|  |  | 4 | 4 to IN |  |
|  | $R 2$ (S27) on main board*** | 1 | 1 to IN |  |
|  |  | 2 | 2 to IN |  |
|  |  | 4 | 4 to IN |  |
|  |  | 8 | 8 to IN |  |
| * The eight dB-value positions of the front-panel rov fac level and $x m t$ fac level DIP switches are cumulative, as are all eight positions of the rev term loss and xmt term loss DIP switches. Total facility-side gain or loss and total terminalside loss introduced into a channel are the sums of that channel's fac level and term loss switch positions set to IN . <br> ** The $1,2,4$, and 8 positions of the SLOPE, $H T$, and $B W$ receive post equalization DIP switches are cumulative. These switch positions may be set in any combination as required. <br> *** All five positions of switch Z (S25), all four positions of switch R2 (S27), the 1,2, and 4 positions of switch R/R1 (S26), and all six positions of switch $\angle B O C(S 8)$ are cumulative. These switch positions may be set in any combination as required. |  |  |  |  |

table 7. Summary and checklist of 6177 alignment switches
receive-channel amplitude equalization
active prescription slope or bump-type equalization for loaded or nonloaded cable, functionally equivalent to that provided by the WECo 309B Prescription Equalizer, with electrical bypass (exclusion) of equalizer available via switch option
terminating impedances, 4 wire ports
1200, 600, or 150 ohms, balanced, individually
switch-selectable at each port
terminating impedance, 2 wire port
900 or $\mathbf{6 0 0}$ ohms in series with $2.15 \mu \mathrm{~F}$, balanced, switch-selectable
frequency response, 4 wire rov to 2 wire, with no equalization and with receive-channel BEF removed
$+0.3,-2.0 \mathrm{~dB}, 200$ to 3000 Hz , re 1004 Hz
$+0.3,-1.3 \mathrm{~dB}, 3000$ to 3400 Hz , re 1004 Hz
frequency response, 2 wire to 4 wire $x m t$
$+0.3,-2.0 \mathrm{~dB}, 200$ to 3000 Hz , re 1004 Hz
$+0.3,-1.3 \mathrm{~dB}, 3000$ to 3400 Hz , re 1004 Hz
compromise balance network (CBN)
switch-selectable for 600 ohms in series with $2.15 \mu \mathrm{~F}$ or $\mathbf{9 0 0}$ ohms in series with $2.15 \mu \mathrm{~F}$
precision balance network (PBN)
integral PBN functionally equivalent to either the WECo 4240B PBN (for nonloaded cable) or the WECo 4240C PBN (for loaded cable), as selected via switch option
line build-out capacitance (LBOC)
O to $0.126 \mu \mathrm{~F}$ in switch-selectable $0.002 \mu \mathrm{~F}$ increments
total harmonic distortion, all ports
less than $1 \%$ at overload points

INCOMING CALL

figure 10. Function sequence flowchart, incoming call

OUTGOING CALL

figure 11. Function sequence flowchart, outgoing call

internal noise, xmt and rcv channels
17 dBrnCO maximum at maximum gain
4wire longitudinal balance
greater than $\mathbf{6 0 d B}, 200$ to $\mathbf{3 0 0 0 H z}$
2wire longitudinal balance
greater than 55dB, 200 to $\mathbf{3 0 0 0 H z}$
4 wire echo return loss
23dB minimum vs. 600 or 1200 ohms
2 wire echo return loss
22dB minimum vs. 600 or 900 ohms in series with $2.15 \mu \mathrm{~F}$
intrinsic transhybrid loss
greater than 35dB ERL
peak-to-average ratio ( $P / A R$ ),
receive-channel BEF removed
98 minimum, without equalization
crosstalk loss between adjacent modules in shelf
80dB minimum, 200 to 3400 Hz

## SF transmit section

internal SF tone oscillator frequency and stability
$2600 \pm 5 \mathrm{~Hz}$ for life of unit
SF tone levels
low level: $-20 \mathrm{dBmO} \pm 1 \mathrm{~dB}$
high level: $-8 \mathrm{dBmO} \pm 1 \mathrm{~dB}$
high-level timing
high-level tone is transmitted for $400 \pm 100 \mathrm{~ms}$ when tone switches from off to on
outgoing SF tone states
see table 3 (loop start) and table 4 (ground start) in section 2 of this practice
pulsing characteristics

- input breaks and makes shorter than 18ms are not recognized
- input breaks between 34 ms and 50 ms are transmitted as $50 \pm 2 \mathrm{~ms}$ tone bursts
- input makes between 18 ms and 25 ms are repeated as $25 \pm 2 \mathrm{~ms}$ silent (no tone) intervals
- input breaks longer than 50 ms are transmitted as tone bursts equal in duration to the input break duration $\pm 2 \mathrm{~ms}$
- input makes longer than $\mathbf{2 5 m s}$ are repeated as silent (no tone) intervals equal in duration to the input make duration $\pm \mathbf{2 m s}$
transmit-path-cut insertion
transmit speech path is cut (opened) $13 \pm 10 \mathrm{~ms}$ before transmission of SF tone
transmit-path-cut removal
transmit speech path cut is removed $125 \pm 50 \mathrm{~ms}$ after detection of an off-hook condition


## SF receive section

SF tone detection
frequency: $2600 \pm 15 \mathrm{~Hz}$
level range: 0 to -27 dBmO
SF tone rejection threshold
$-37 \mathrm{dBm0}$
signal-to-guard ratio for signal detection
6 to 12dB
incoming SF tone states
see table 3 (loop start) and table 4 (ground start) in section 2 of this practice
maximum line noise
51dBrnCo
guard circuit transition timing
high-to-low: $\mathbf{2 2 5} \pm 60 \mathrm{~ms}$
low-to-high: $\mathbf{5 0} \pm 10 \mathrm{~ms}$
band-elimination-filter timing

- insertion time: $13 \pm 7 \mathrm{~ms}$
- insertion duration for SF tones shorter than $175 \pm 60 \mathrm{~ms}$ : $225 \pm 50 \mathrm{~ms}$ (with BEF insertion duration longer than tone duration in all cases)
- insertion duration for SF tones longer than $175 \pm 60 \mathrm{~ms}$ : duration of SF tone plus $\mathbf{5 0} \pm 10 \mathrm{~ms}$
seizure delay (incoming)
loop-start mode: $225 \pm 60 \mathrm{~ms}$
ground-start mode: $150 \pm 50 \mathrm{~ms}$
release delay (incoming)
$250 \pm 50 \mathrm{~ms}$


## 2wire loop conditions

maximum loop resistance
3000 ohms with -48 Vdc input battery
maximum 2 wire loop current (current-limited) $35 \pm 5 \mathrm{~mA}$ with -48 Vdc input battery

## external ringing supply requirements

frequency
16 to 67 Hz
bias
must be referenced to negative battery supply
level
130Vac maximum

## traffic-monitoring (sleeve) lead

traffic-monitoring (sleeve) lead states
idle condition: open circuit (diode clamped to negative input potential)
busy condition: ground ( 100 mA maximum source capacity)

## common specifications

input power requirements
voltage: - 42 to $\mathbf{- 5 4 V d c}$, filtered, positive-ground referenced
idle current: 75 mA typical at -48 Vdc
busy current: 126 mA maximum at -54 Vdc , not including loop current and with one channel at maximum output
operating environment
$32^{\circ}$ to $122^{\circ} \mathrm{F}\left(0^{\circ}\right.$ to $\left.50^{\circ} \mathrm{C}\right)$, humidity to $95 \%$
(no condensation)
dimensions
5.58 inches ( 14.17 cm ) high
1.42 inches ( 3.61 cm ) wide
5.96 inches ( 15.14 cm ) deep
weight
13 ounces ( 369 grams)
mounting
relay rack or apparatus case via one position of a
Tellabs Type 10 Mounting Shelf

## 7. testing and troubleshooting

7.01 The troubleshooting guide in this section may be used in conjunction with the function sequence flowcharts (figures 10 and 11) in section 4 of this practice to assist in the installation, testing, or troubleshooting of the 6177 4Wire-to-2Wire SF-to-FXS Intermediate Repeater module. The guide is intended as an aid in the localization of trouble to a specific module. If a module is suspected of being defective, a new one should be substituted and the test conducted again. If the substitute module operates correctly, the original module should be considered defective and returned to Tellabs for repair or replacement. We strongly recommend that no internal (component-level) testing or repairs be attempted on the module. Unauthorized testing or repairs may void the module's warranty. Also, if the module is part of a registered system, unauthorized repairs will result in noncompliance with Part 68 of the FCC Rules and Regulations.
Note: Warranty service does not include removal of permanent customer markings on the front panels of Tellabs modules, although an attempt will be made to do so. If a module must be marked defective, we recommend that it be done on a piece of tape or on a removable stick-on label.
7.02 If a situation arises that is not covered in the troubleshooting guide, contact Tellabs Customer Service as follows (telephone numbers are given below):
USA customers: Contact Tellabs Customer Service at your Tellabs Regional Office.
Canadian customers: Contact Tellabs Customer
Service at our Canadian headquarters in Mississauga, Ontario.
International customers: Contact your Tellabs distributor.

US Atlantic Region: (203) 798-0506
US Capital Region: (703) 478-0468
US Central Region: (312) 357-7400
US Southeast Region: (305) 834-8311
US Southwest Region: (214) 869-4114
US Western Region: (714) 850-1300
Canada: (416) 624-0052
7.03 If a module is diagnosed as defective, follow the replacement procedure in paragraph 7.04 when a critical service outage exists (e.g., when a system or a critical circuit is down and no spares are available). If the situation is not critical, follow the repair and return procedure in paragraph 7.05 .

## replacement

7.04 To obtain a replacement module, notify Tellabs via letter or telephone (see addresses and numbers below) or via TWX (910-695-3530 in the USA, 610-492-4387 in Canada). Be sure to provide all relevant information, including the $8 \times 6177$ part number that indicates the issue of the module in question. Upon notification, we shall ship a replacement to you. If the module in question is in warranty, the replacement will be shipped at no charge. Pack the defective module in the replacement's carton, sign the packing slip included with the replacement, and enclose it with the defective module (this is your return authorization). Affix the preaddressed label provided with the replacement module to the carton being returned, and ship the carton prepaid to Tellabs.

## repair and return

7.05 Return the defective 6177 module, shipment prepaid, to Tellabs (attn: repair and return).
in the USA:
Tellabs, Inc.
4951 Indiana Avenue
Lisle, Illinois 60532
telephone: (312) 969-8800
in Canada:
Tellabs Communications Canada, Ltd.
1200 Aerowood Drive, Unit 39
Mississauga, Ontario, Canada L4W 2S7
telephone: (416) 624-0052
Enclose an explanation of the module's malfunction. Follow your company's standard procedure with regard to administrative paperwork. Tellabs will repair the module and ship it back to you. If the module is in warranty, no invoice will be issued.


[^0]:    Note: On early versions of this module, the $I N$ setting for the $Z$ and $R / R 1$ DIP switches (S25 and S26) is down, i.e., toward the main printed circuit board. On later versions of the module, the $/ \mathrm{N}$ setting for these switches is up, i.e., toward the baby board, as shown in figure 9 .

